

“Condition Monitoring and Vibration Signal measurement of of Rolling Contact Bearing”

Sawai Mandakini
PG Scholer
SVCET Rajuri Pune

Prof. Randhvan Bhagwat
Assistant Professor
SVCET Rajuri Pune

Abstract- In this paper, an investigation of the condition observing of the roller contact bearing is introduced. Bearing example information comprises of four unique circumstances as having flawed internal race, deficient external race, having deserts on roller and a solid bearing. For the readiness of the example bearing, laser machine is utilized for presentation of the miniature size deserts on the surfaces. A startling disappointment of the moving contact bearing might cause huge monetary misfortunes. Therefore, shortcoming conclusion in bearing has been the subject of serious examination. Vibration signal examination has been broadly utilized in the shortcoming recognition of pivot apparatus. The vibration sign of a moving contact bearing conveys the mark of the shortcoming in the bearing, and early issue identification of the bearing is conceivable by examining the vibration signal utilizing different sign handling procedures. From that vibration estimation strategy is generally utilized in the business for condition checking of various hardware and it tends to have the option to identify 92% of deficiencies or disappointment in the machines by the adjustment of vibration signals. Consequently it is vital to comprehension of the vibration signals related with moving component orientation.

Keywords: Condition Monitoring, FFT, Rolling Contact Bearing, Fault Analysis

I. INTRODUCTION

In present time, administrations, plans and assembling of mechanical frameworks enjoy benefit of PCs and computerization for quick, precise and productive result. Pivoting hardware is utilized in fast apparatus because of its adjusting advantage over the responding hardware. Bearing is most usually utilized significant part to be found in all pivoting hardware. It is observed structure bike to super apparatus and helicopter. Bearing is giving relative movement between help bodies and pivoting part and furthermore communicate the heap to the base. So bearing is vital piece of hardware. There are many purposes behind the wear and disappointment of direction. Primary drivers of disappointment are the high pivoting speeds, over load and extreme working circumstances. Heading are creating the vibration during activity. The other potential wellsprings of the moving component bearing vibrations are the imperfections of the moving heading, unbalance burden and misalignments. For understanding working state of the bearing, creating advance numerical model for genuine application is significant. To comprehend the elements working state of bearing for such an application it's becomes troublesome in view of radial powers following up on the moving components, material properties and the slipping of the moving components as they roll on the race. There are ordinary and current methods of the distinguishing states of the direction. From that vibration estimation method is broadly utilized in the business for condition checking of

various apparatuses and it very well may have the option to identify 92% of flaws or disappointment in the machines by the adjustment of vibration signals. Along these lines it is vital to comprehension of the vibration signals related with moving component direction.

A. Common Causes of Bearing Failures

Unfamiliar matter is one of most normal reason in bearing is wear and pitting. This sort of imperfection might be distinguished by irregular commotion from the bearing during activity.

- Bearing Fatigue When bearing is turned the moving part rolls and changes its situation in various stacking zone.
- Long-lasting twisting brought about by abrupt effect load during working condition or weighty stacking during revolution of bearing.
- Erosion in bearing is brought about by the substance assault on the bearing metal by presence water and acids in working climate.
- High Temperature of bearing is expands because of unreasonable intensity age or unfortunate intensity evacuation (grease) structure the bearing.
- Inappropriate Installation Bearing internal race and shaft is collected in press or obstruction fit.
- Ill-advised oil Lack of oil or wrong choice of grease results the overheating.
- Plastic twisting happens between reaching surfaces when unreasonable fixed burden or effect load is applied during rest condition.

B. Dynamics Of Bearing

Elements of the bearing comprises of the investigation of the powers following up on the various components of the bearing during activity. The powerful demonstrating of the bearing for elite execution applications is complicated and non-straight in nature. This non-linearity is because of the material nonlinearity, mathematical non-linearity and kinematic non-linearity. Non-direct demonstrating of bearing is to be more sensible under severe circumstances.

Whenever an actual framework is broke down, its way of behaving can be displayed in a numerical structure as a situation. On the off chance that the framework is accepted to act as straight; a direct condition can be utilized to communicate this framework. On the off chance that the framework is accepted to act as nonlinear, the condition which addresses the framework will be non-direct. Tackling a non-straight differential condition is considerably more intricate than settling a direct differential condition. Non-



straight conditions can be tackled by normal rough techniques or by simply mathematical strategies.

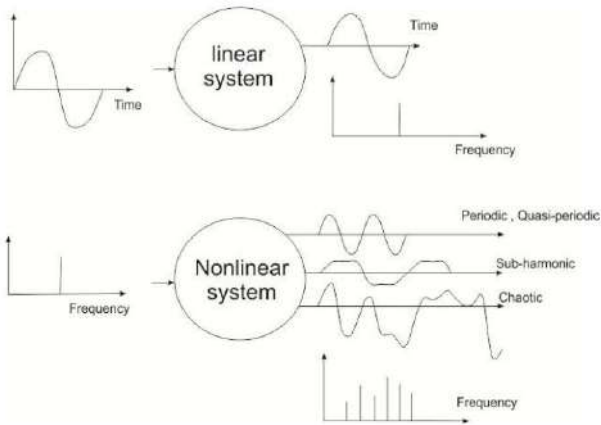


Fig. 1. Input output for linear and nonlinear system of bearing.

II. BEARING CONDITION MONITORING

In present period of rivalry, any ventures can't make due assuming there separate time is high because of disappointment of any part of hardware. To keep up with the great shape of apparatus, businesses utilized different upkeep procedures. The motivation behind support is keeping hardware and plant at high unwavering quality, protected and steady. This will result ventures productive. The essential sorts of support methods are breakdown upkeep and preventive upkeep. Breakdown upkeep was not utilized by ventures because of west of time and cash. Preventive systems for upkeeps further delegated support on fixed time or routine upkeep, opportunity support and condition based support. Condition checking is one of most power full preventive upkeep techniques. Vibration based Condition Monitoring is a fundamental piece of Predictive Maintenance, Vibration based condition observing involves three principal stages; shortcoming location, analytic and forecast. The principal issue in bearing shortcoming diagnostics is the capacity to recognize and identify flaws as soon as could really be expected. Information procurement framework is then expected to record the vibration mark of the frameworks and signs should have been placed into a structure where significant data can be removed. Time space, recurrence area and time-recurrence space examinations are the normal strategies for dissecting vibration signals for separating valuable element about shortcoming. From the time area examination typically figure out indiscreet motions, similar to root mean square worth, top worth, crest variable and minutes like kurtosis. It contains the data when it works out. In recurrence area investigation, different frequencies extricated from vibration signal like regular recurrence, trademark shortcoming frequencies and its sounds by various change techniques. It gives data what works out. For getting benefit of what occurs and when happen time-recurrence space examination procedures where utilized. Completing this investigation physically has its own constraints.

A. Objective Of The Study

Limited number of moving components pivoting with various speeds as for the inward race, produce a period fluctuating solidness part.

These limited moving contacts between the moving components and the directing races present a serious level of non-linearity in the heading, which brings about a nonlinear unique way of behaving of the framework.

Moreover, the impact of the faulty course on the vibration mark is likewise explored by mathematically and approved those vibration marks by exploratory outcomes.

Reaction surface technique (RSM) is utilized to examine the vibration reaction under the impacts of the confined deformities all the while, spiral burden, speed and the communications among them.

III. NON LINEAR MODEL OF CYLINDRICAL ROLLER BEARING

Actual powerful reaction of barrel shaped roller bearing is required for the comprehension the way of behaving of imperfection free bearing. Hertzian contact force is considered as a wellspring of non-linearity concerning creating numerical model. The boundaries of study are rotational speed of rotor, size of deformity and spiral burden.

For a numerical model for the underlying vibrations in roller bearing has been created as spring mass damper framework. In outspread course consistent power thought to be following up on the framework due to pivoting mass minding by rotor.

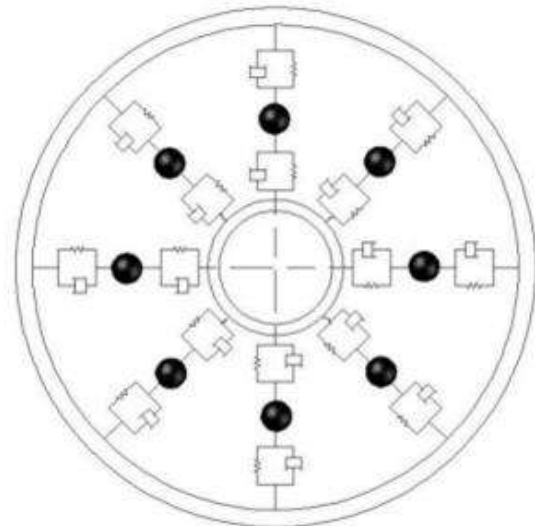


Fig. 2. rolling element bearing as spring, mass and damper system

Contact between the rolling surfaces assume to be non-linear contact spring and damper. To develop the mathematical model some assumptions are considered such as according to the elastic contact Hertzian theory deformation is occur, same motion in plane, angular velocity of case remains constant.

$$\text{Shaftor inner race angular speed } \omega_2 = \frac{2\pi N}{60}$$

$$\text{Velocity of inner race } v_i = \omega_2 \times R_i$$

$$\text{Velocity of outer Race } v_o = 0$$

$$\text{Velocity of case } V_c = (v_i + v_o)/2$$

$$\text{Velocity of cage } V_c = v_i/2$$

$$\text{Angular velocity of case is } V_c = (v_c) \times 2/(R_i + R_o)$$

Contact Spring force

empirical relation for roller contact bearing have developed by Palmgren(1959) with considering contact force acting and deformation occurs at the line contact of roller and races[1]

$$\delta = 3.84 \times 10^{-5} \times \frac{Q^{0.9}}{1^{0.8}}$$

Generalized linear equation for dissipative force is

$$F_d = c \dot{\delta}$$

To find spring force and dissipative force, first we required to find the deformation (δ) and its time derivative.

Total roller raceway deformation = [Contact deformation due to radial load] + [Radial deflection due to thrust loading] – [Radial clearance between contact surface] – [localized defect].

Contact deformation due to radial load is considered uniformly distributed along the length of contact.***. Radial deflection and axial deflection is also cause of axial thrust. (Harris and Kotzalas, 2006Harris and Kotzalas, 2006*****)

Total load on j^{th} roller with considering unit length λ^{th} is derived as follows:

$$Q_j = \sum_{i=1}^{i=k} \frac{[\Delta_j + w \left(\lambda - \frac{1}{2} \right) \zeta_j - \frac{P_d}{2} - P]^{1.11}}{1.24 \times 10^{-5} \times k^{0.11}} \times w^{0.89}$$

Formulation of localized defect consider descriptions of shapes of localized defects are known as per classification of local defects. For the modeling of local defect, *****Harsha (2006) [21,22] consider the movement of rolling contact with the rolling surfaces were sinusoidal

Equilibrium Equation in static condition With considering static equilibrium of radial and trust load

following two equilibrium equations were derived as (Harris, 2006) [129],

In equilibrium condition, total radial deflection due to radial loading and radial deflection due to axial deflection caused by the axial load is equal to sum total race way deflection due to contact deformation. the equation of static equilibrium is,

$$\left[\delta_a \times \frac{1}{D} \right] + [\delta_r \cos \psi_j] - \frac{P_d}{2} - 2 \sum_{i=1}^{i=k} \left[\Delta_j + w \left(\lambda - \frac{1}{2} \right) \zeta_j - \frac{P_d}{2} - P \right] = 0$$

For find out total raceway deformation of bearing, set of nonlinear equations which can be solve for four unknown $[\Delta_j, \zeta_j, \delta_a, \delta_r]$ for each of roller.

Several methods are available for solving nonlinear equations. Some iterative methods like Newton-Raphson, Secant, Muller’s, Birstow’s and fixed point methods are available for solving non-linear equations. In these methods use a single starting value that do not necessary the root. Newton-Raphson method is use to solve above equation for finding out deformations for each rollers.

IV. SIMULATION OF MODEL

To notice the impact of rotational speed and limited deformity, hardly any results at different velocities were gotten in vertical and even headings through recreated numerical model and it is conduct is examined. The reactions are acquired in recurrence area with Poincare maps. The recreation recurrence is contrasted and determined frequencies of existing model for same working condition. NJ 305 bearing is considered for recreation of numerical model. Same bearing is utilized for exploratory work.

Table use

TABLE I. INNER AND OUTER RACE RESPONSES OF MATHEMATICAL MODELLING IN VERTICAL AND HORIZONTAL DIRECTIONS

SN	Race	Rotor Speed (rpm)	rotor frequency (ω_2)	compliance frequency (Hz)	ball passage frequency on the outer race (ω_{bpf_i}),
By Calculation Based					
1	Inner	1000	16.6	66.21	100.45
		1500	30	119	180.81
2	outer	1440	23.3	92.7	92.7
		1500	30	119	180.81
3	Rotor Speed (rpm)		Directions	ball passage frequency on the outer race (ω_{bpf_i}),	Aptitudes (μm)
Response of Inner race defect size 0.5 mm					
5	1000	Vertical	100	5.2	
			190	7.8	
			115	6.9	
		Horizontal	100	5.2	
			190	5.4	
			115	5.6	
5	1500	Vertical	200	6	
			115	4.7	
			30	2.6	
		Horizontal	200	5.0	
			27	5.1	
			115	5.6	
Response of Outer race defect size 0.5 mm					
6		Horizontal	93	4.5	
			169	4.7	
		Horizontal	110	2.5	
			145	2.85	

From the determined recurrence and trademark issue frequencies show up in reproduced results are very closer. For the inward race deformity the frequencies shows up at music of shortcoming recurrence too. Furthermore, for the external race imperfection frequencies shows up at amount of the trademark shortcoming recurrence and rotational recurrence of rotor or inward race.

Innert Race Defect;

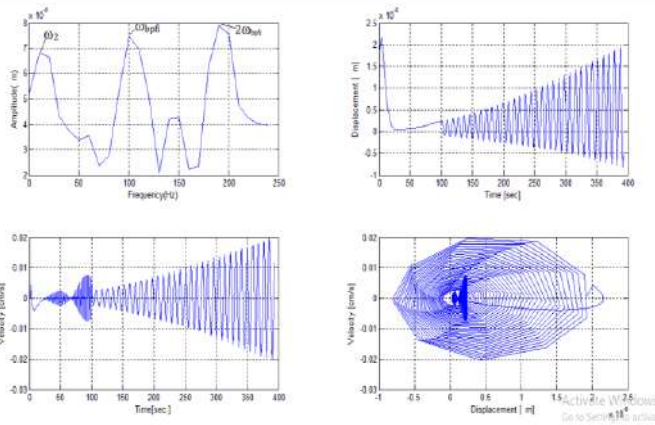


Fig. 3. Response in Vertical direction of bearing with Inner race defect at 1000 rpm.

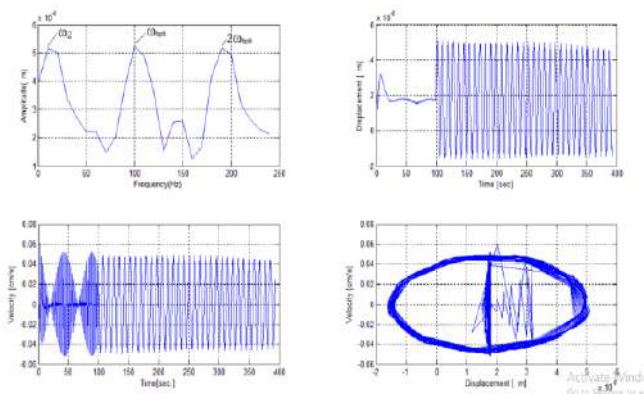


Fig. 4. Response in Horizontal direction of bearing with Inner race defect at 1000 rpm

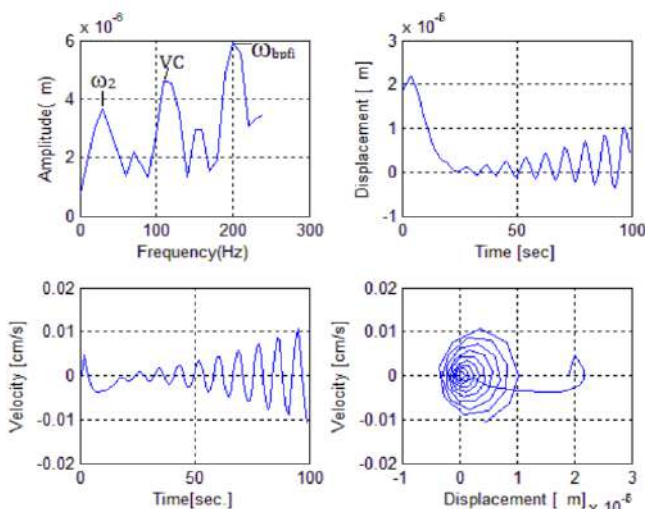


Fig. 5. Response in vertical direction of bearing with Inner race defect at 1800 rpm.

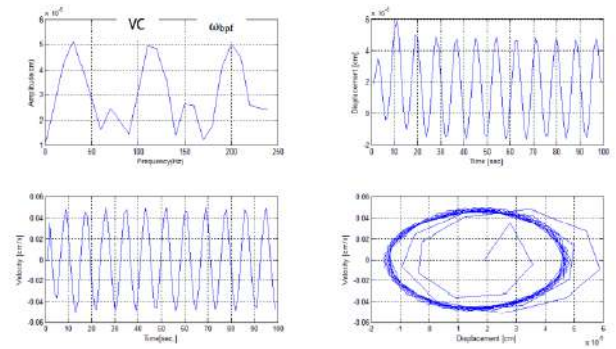


Fig. 6. Response in Horizontal direction of bearing with Inner race defect at 1800 rpm.

Response of Outer race defect

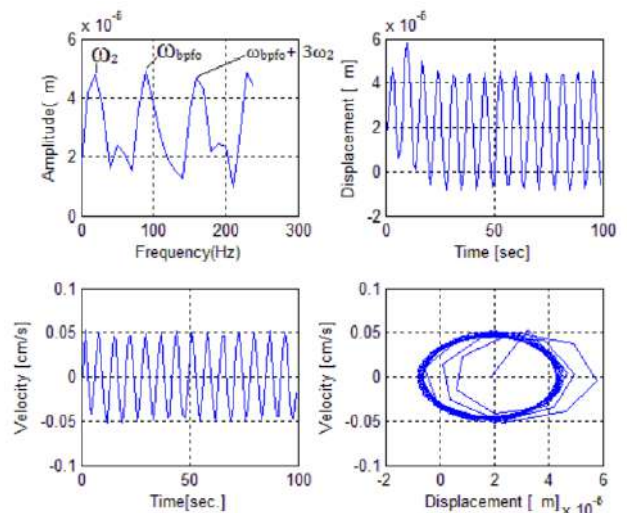


Fig. 7. Response in Horizontal direction of bearing with outer race defect at 1400 rpm.

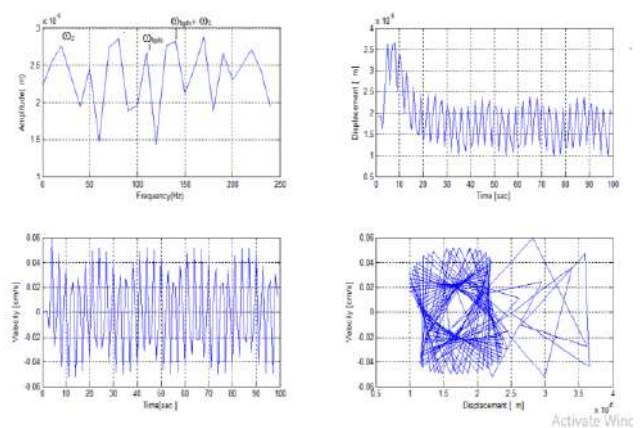


Fig. 8. Response in Horizontal direction of bearing with Inner race defect at 1800 rpm.

V. EXPERIMENTAL WORK

Vibration signal is caught from various turning velocity and afterward Response Surface Method is utilized to figure out the adequacy of working boundaries and deformities on activity execution of bearing. With the assistance of information securing framework record the vibration mark of the framework and signals should be placed into a structure where significant data can be extricated. the exploratory test rig has been created in vibration research facility. A shaft is

upheld on moving component direction and driven by an AC engine. The rotor (plate) is mounted on 28 mm measurement shaft. The speed of the shaft is differed and constrained by factor recurrence drive. An adaptable coupling has been utilized to interface rotor shaft and engine to repay any misalignment. The even shaft of weight 2 kg is utilized and rig is associated with an information obtaining framework through appropriate instrumentation.

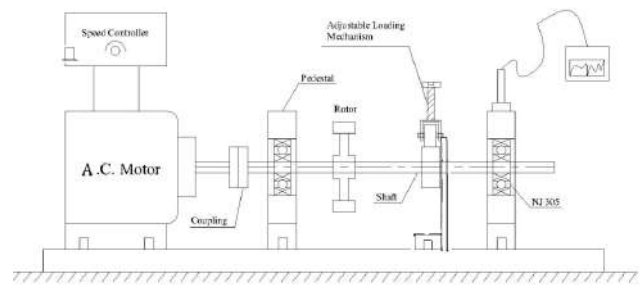
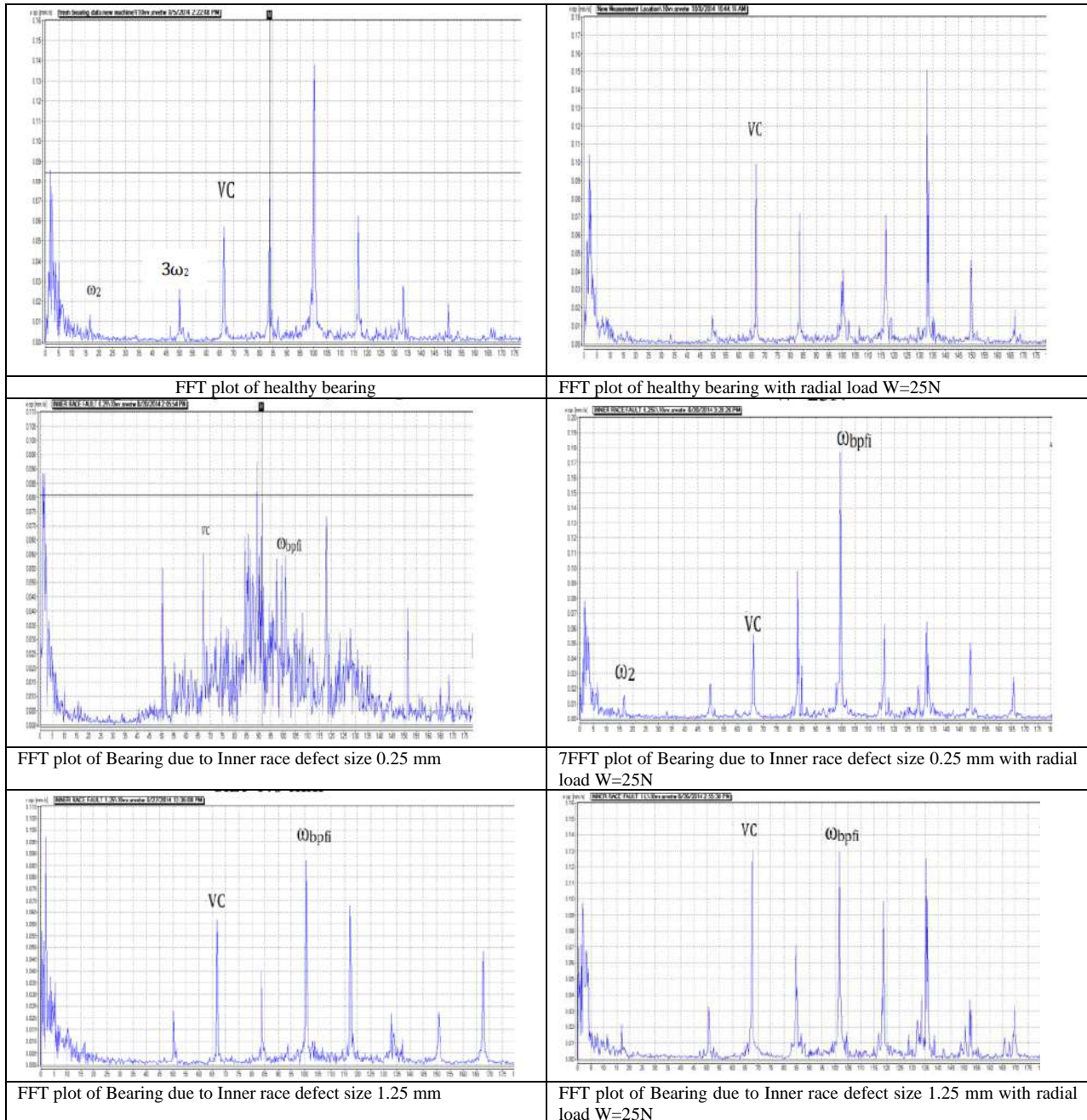
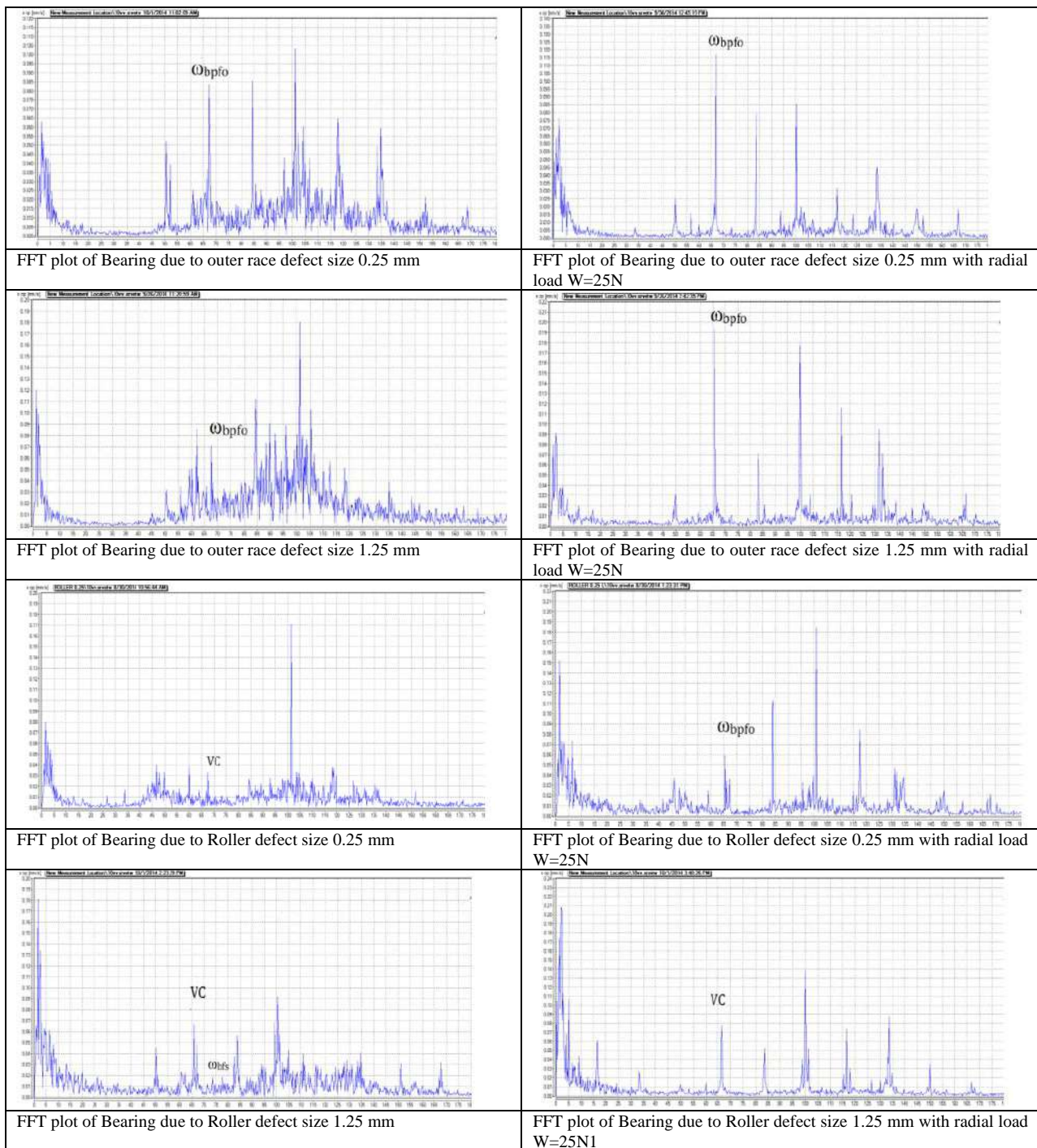


Fig. 9. Schematic diagram of Experimental set up





From the gathered information of various restricted flaws at different speed and stacking condition, No tremendous change in plentifulness is seen in load and no heap condition for sound bearing. FFT chart for internal race imperfection size 0.25 mm and 1.25mm in sync of 0.25 mm for no heap and with spiral burden are displayed in figure, The reaction recurrence chiefly shows up at entry recurrence on inward race ω_{bpfi} and differing consistence recurrence for inward race issue. For inward race imperfection size 0.25 mm, the abundance of speed in vertical headings is 0.06 mm/sec. what's more, 0.18 mm/sec. For external race deformity, the FFT outlines of imperfection size 0.25mm and 1.25 mm with load and without load is displayed in Fig.

VI. CONCLUSION:

From the trial work and numerical model of a roller, because of limited deformity the succeeding discoveries might be anticipated. With increase in deformity size the sufficiency of vibrations is expanded and afterward diminishes because of "self-Peening" impact. Furthermore, with augmentation of rotational speed with confined imperfection the attributes deformity recurrence likewise moved on FFT graph and the way of behaving of activity is change from intermittent to turbulent. For individual restricted absconds on internal race, roller and external race, the pinnacles show up at attributes issue frequencies. The trademark shortcoming frequencies show up with

communication with case recurrence and ball entry frequencies in joined restricted issues.

REFERENCES

- [1] ADASH Dewesoft, Manuals & Brochures, 2020.
- [2] S. Singh, C.Q. Howard, C.H. Hansen, An extensive review of vibration modeling of rolling element bearings with localized and extended defects, *J. Sound Vib.* 357 (2015) 300–330, <https://doi.org/10.1016/j.jsv.2015.04.037>.
- [3] H. Cheng, Y. Zhang, W. Lu, Y. Zhou, Research on ball-bearing model based on local defects, *SN Appl. Sci.* 1 (2019) 1219, <https://doi.org/10.1007/s42452-019-1251-4>.
- [4] T. Govardhan, A. Choudhury, D. Paliwal, Vibration analysis of dynamically loaded bearing with distributed defect based on defect induced excitation, *Int. J. Dynam. Control* (2017) 1–12, <https://doi.org/10.1007/s40435-017-0324-8>.
- [5] T. Govardhan, A. Choudhury, Fault Diagnosis of Dynamically Loaded Bearing with Localized Defect Based on Defect-Induced Excitation, *J. Fail. Anal. Prev.* 19 (2019) 844–857, <https://doi.org/10.1007/s11668-019-00668-0>. Fig. 12. Comparisons of the vibration responses (a) experimental (b) simulated. Table 8 Comparison between the model and the empirical results of the rotor-bearing system. Sr. No. Experimental Results Simulated Results Frequency (Hz) Amplitude (m/ s²) Frequency (Hz) Amplitude (m/ s²)
1 22.8 0.005 22.9 0.006 2 26.9 0.018 26.9 0.021 3 31.2 0.009 31 0.008 4 54.1 0.019 53.8 0.021 5 58.3 0.015 57.8 0.018 G.L. Suryawanshi et al. *Measurement* 184 (2021) 109879 10
- [6] D. Chandra, Y. Rao, Fault Diagnosis of a Double-Row Spherical Roller Bearing for Induction Motor Using Vibration Monitoring Technique, *J. Fail. Anal. Prev.* 19 (2019) 1144–1152, <https://doi.org/10.1007/s11668-019-00712-z>.
- [7] W. Zi, C. Zhu, A new model for analyzing the vibration behaviors of the rotorbearing system, *Commun. Nonlinear Sci. Numer. Simul.* 83 (2020), 105130, <https://doi.org/10.1016/j.cnsns.2019.105130>.
- [8] P. Gao, L. Hou, R. Yang, Y. Chen, Local defect modeling and nonlinear dynamic analysis for the inter-shaft bearing in a dual-rotor system, *Appl. Math. Model.* 68 (2019) 29–47, <https://doi.org/10.1016/j.apm.2018.11.014>.
- [9] Y. Jiang, W. Huang, J. Luo, W. Wang, An improved dynamic model of defective bearings considering the three-dimensional geometric relationship between the rolling element and defect area, *Mech. Syst. Sig. Process.* 129 (2019) 694–716, <https://doi.org/10.1016/j.ymsp.2019.04.056>.
- [10] L. Niu, H. Cao, H. Hou, B. Wu, Y. Lan, X. Xiong, Experimental observations and dynamic modeling of vibration, characteristics of a cylindrical roller bearing with roller defects, *Mech. Syst. Sig. Process.* 138 (2020), <https://doi.org/10.1016/j.ymsp.2019.106553>.
- [11] Y. Liu, Y. Zhu, K. Yan, F. Wang, J. Hong, A novel method to model effects of natural defect on a roller bearing, *Tribol. Int.* 122 (2018) 169–178, <https://doi.org/10.1016/j.triboint.2018.02.028>.
- [12] Y. Yang, W. Yang, D. Jiang, Simulation and experimental analysis of rolling element bearing fault in the rotor-bearing-casing system, *Eng. Fail. Anal.* 92 (2018) 205–221, <https://doi.org/10.1016/j.engfailanal.2018.04.053>.
- [13] I.El Thalji, E. Jantunen, Fault analysis of the wear fault development in rolling bearings, *Eng. Failure Anal.* 57 (2015) 470–482, <https://doi.org/10.1016/j.engfailanal.2015.08.013>.
- [14] D.S. Shah, V.N. Patel, A dynamic model for vibration studies of dry and lubricated deep groove ball bearings considering local defects on races, *Measurement* 137 (2019) 535–555, <https://doi.org/10.1016/j.measurement.2019.01.097>.
- [15] Z. Shi, J. Liu, An improved planar dynamic model for vibration analysis of a cylindrical roller bearing, *Mech. Mach. Theory* 153 (2020), 103994, <https://doi.org/10.1016/j.mechmachtheory.2020.103994>.
- [16] H. Cao, D. Wang, Y. Zhu, X. Chen, Dynamic modeling and abnormal contact analysis of rolling ball bearings with double half-inner rings, *Mech. Syst. Sig. Process.* 147 107075, DOI: 10.1016/j.ymsp.2020.107075.
- [17] Y. Xiaolan, Y. Liu, M. Jia, Research on an enhanced scale morphological-hat product filtering in incipient fault detection of rolling element bearings, *Measurement* 147 (2019), 106856, <https://doi.org/10.1016/j.measurement.2019.106856>.
- [18] T. Guiji, X. Wang, Y. He, Diagnosis of compound faults of rolling bearings through adaptive maximum correlated kurtosis deconvolution, *J. Mech. Sci. Technol.* 30 (1) (2016) 43–54, <https://doi.org/10.1007/s12206-015-1206-7>.
- [19] R.G. Desavale, R. Venkatachalam, S.P. Chavan, Experimental and numerical studies on spherical roller bearings using multivariable regression analysis, 021022–1–10, *J. Vib. Acoustics* 136 (2014), <https://doi.org/10.1115/1.4026433>.
- [20] R.G. Desavale, R.A. Kanai, S.P. Chavan, R. Venkatachalam, P.M. Jadhav, Vibration Characteristics Diagnosis of Roller Bearing Using the New Empirical Model, *J. Tribol.* 138 (2016), 011103, <https://doi.org/10.1115/1.4031065>.